

# **Heat Sink Welding for Preventing Hot Cracking in Alloy 2195 Intersection Welds: A Feasibility Study**

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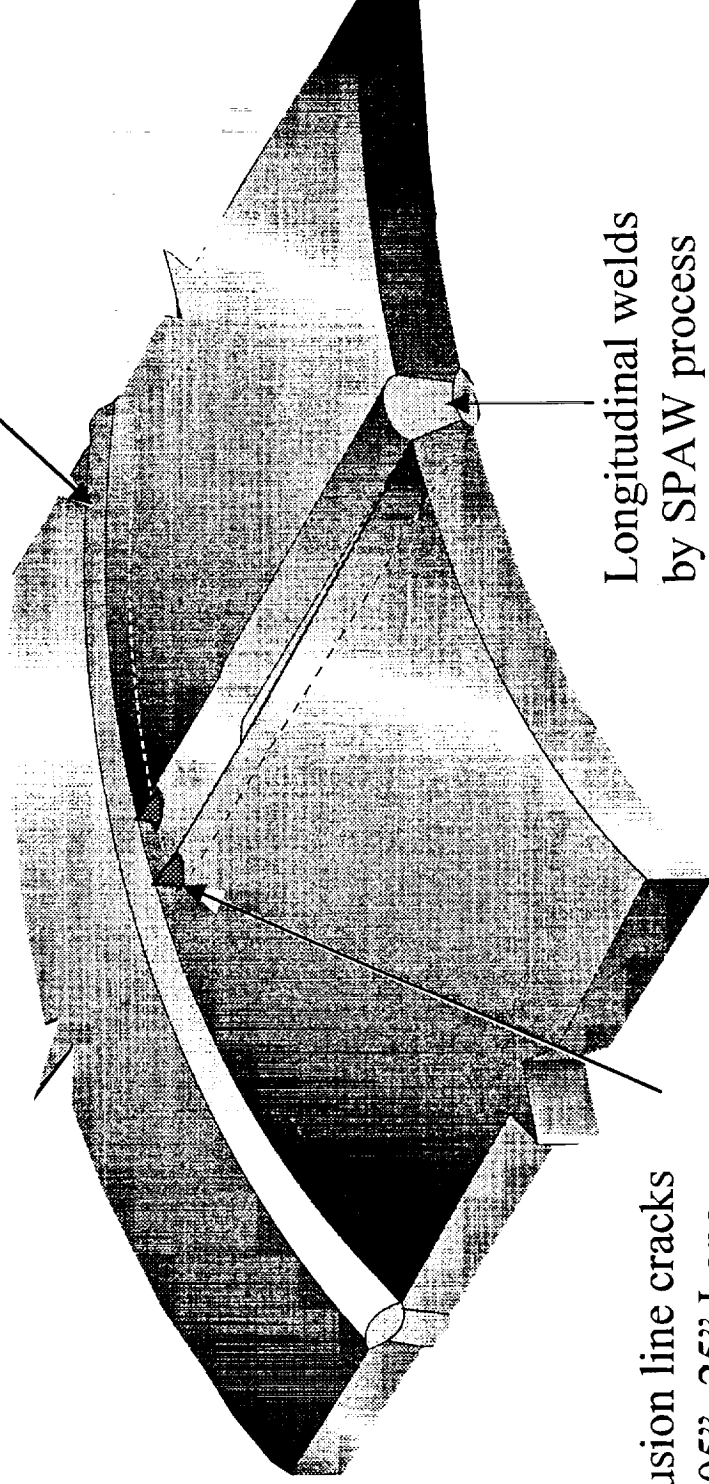
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# Potential Weld Crack Sites of Concern

Circumferential welds  
by SPAW process

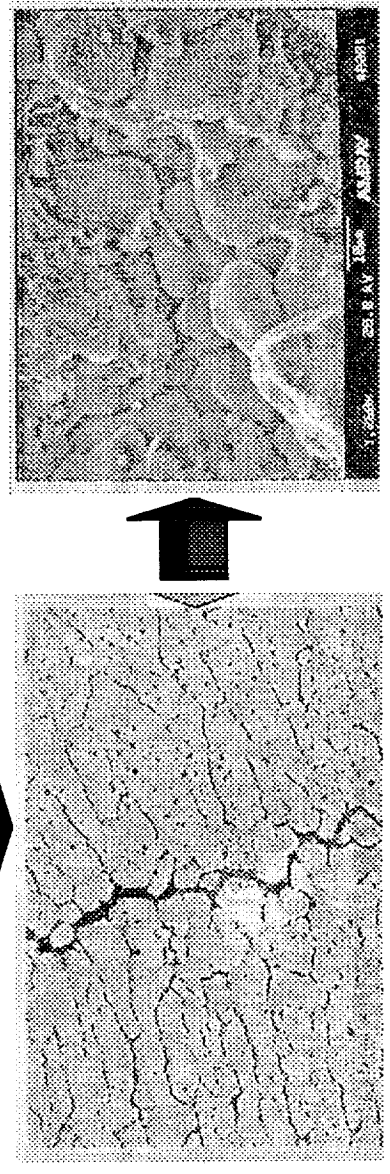
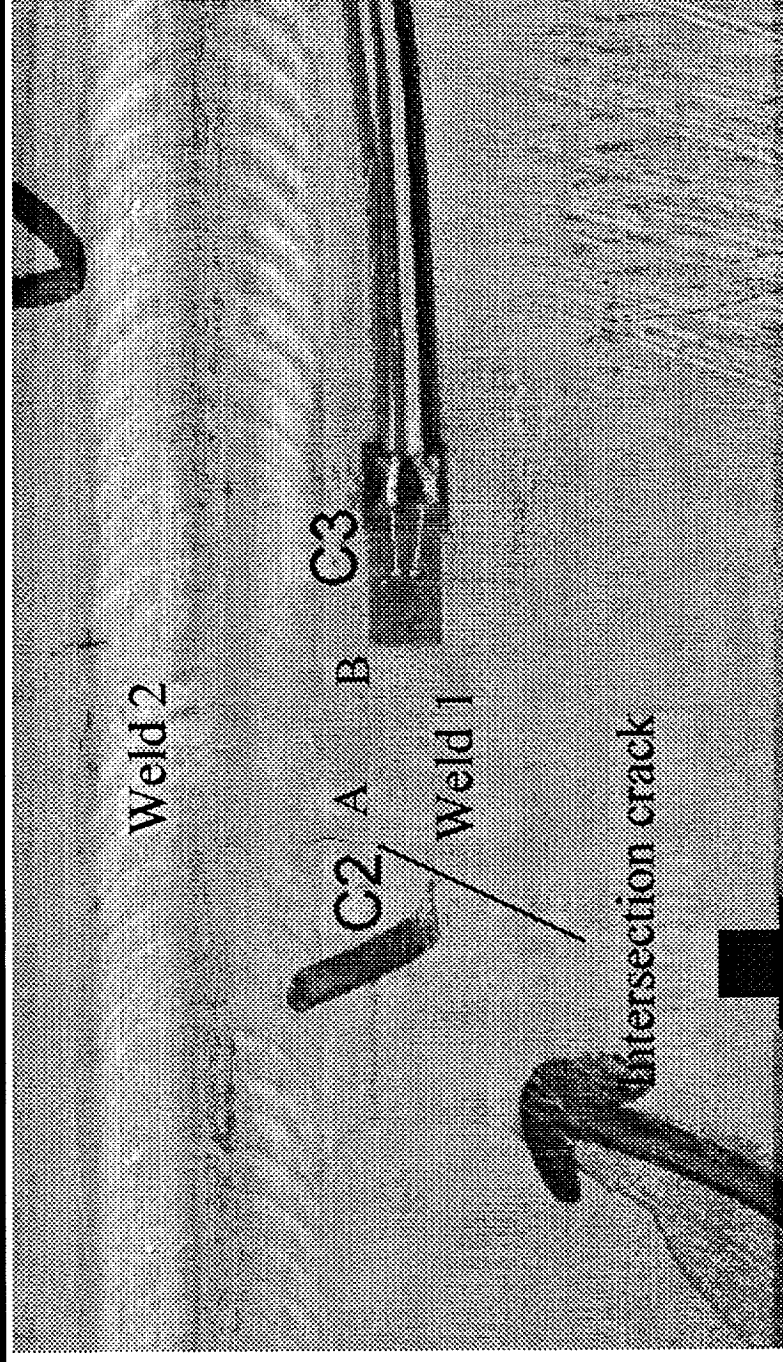
Longitudinal welds  
by SPAW process

Fusion line cracks  
0.05"-.25" Long  
0.50"-.20" Deep



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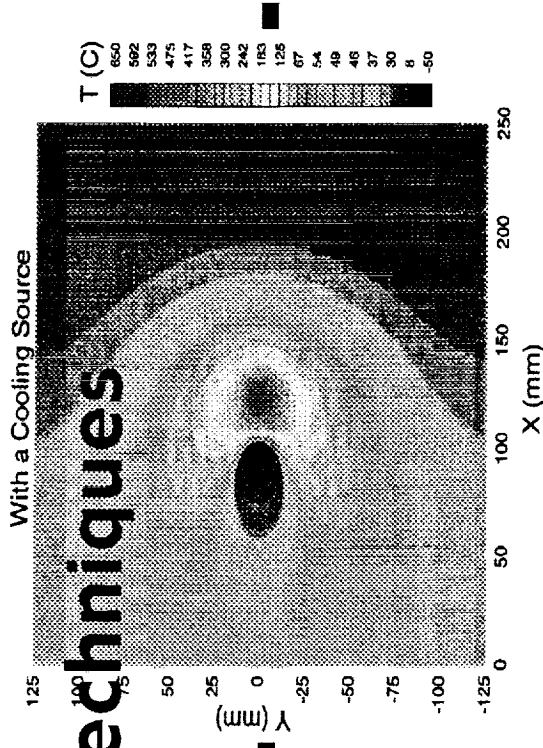
# Intersection Crack - A Test Panel Weld



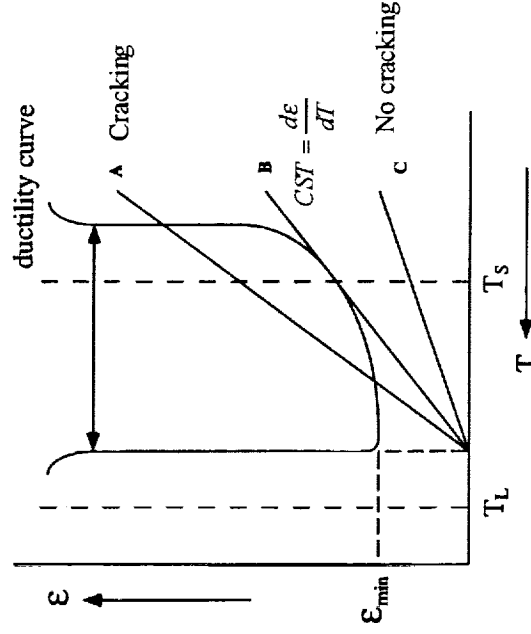
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# Hot-Cracking Mitigation Techniques

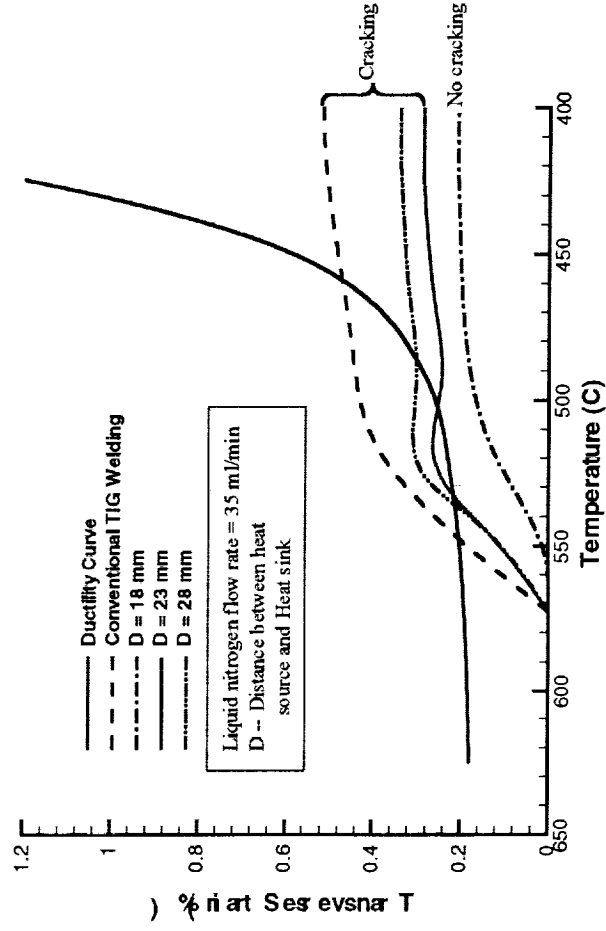
## with a Heat Sink



(b) Temperature Distribution welding with a Heat Sink



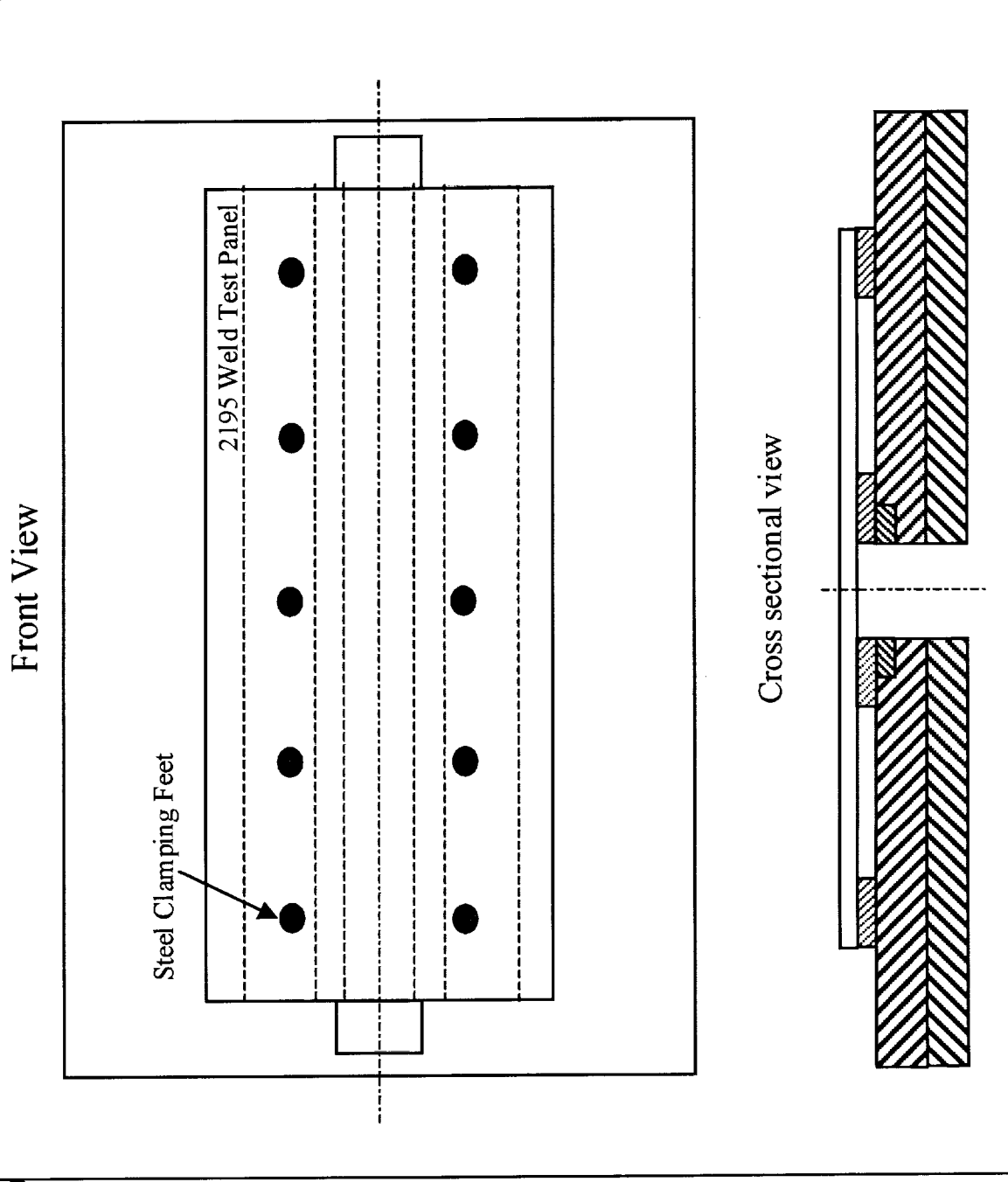
(a) Thermomechanical Conditions Associated with Hot Cracking



(c) Effects of Heat Sink on Development of Tensile Strain

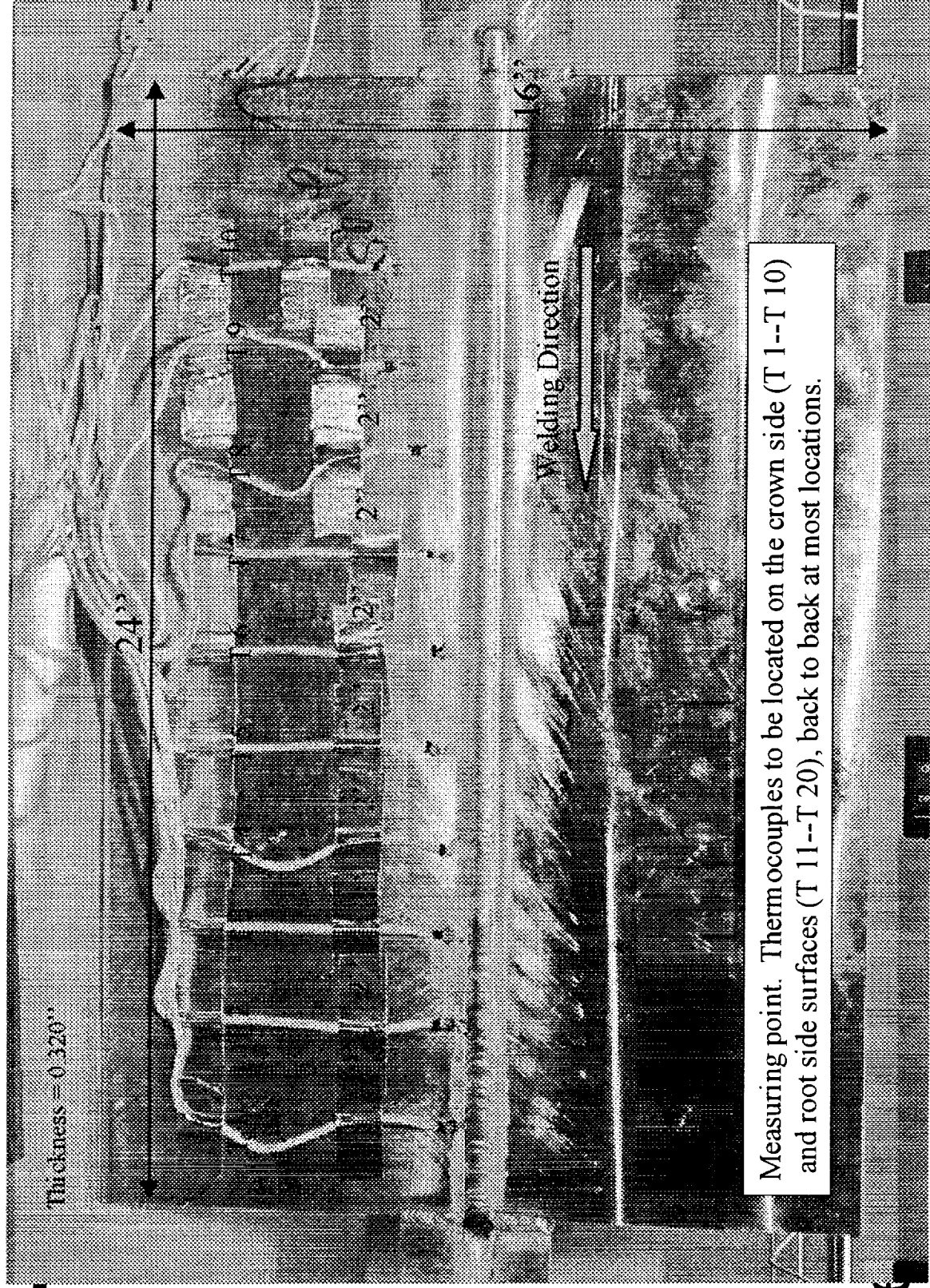
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# Weld Test Panel and Fixture for thermocouple panels



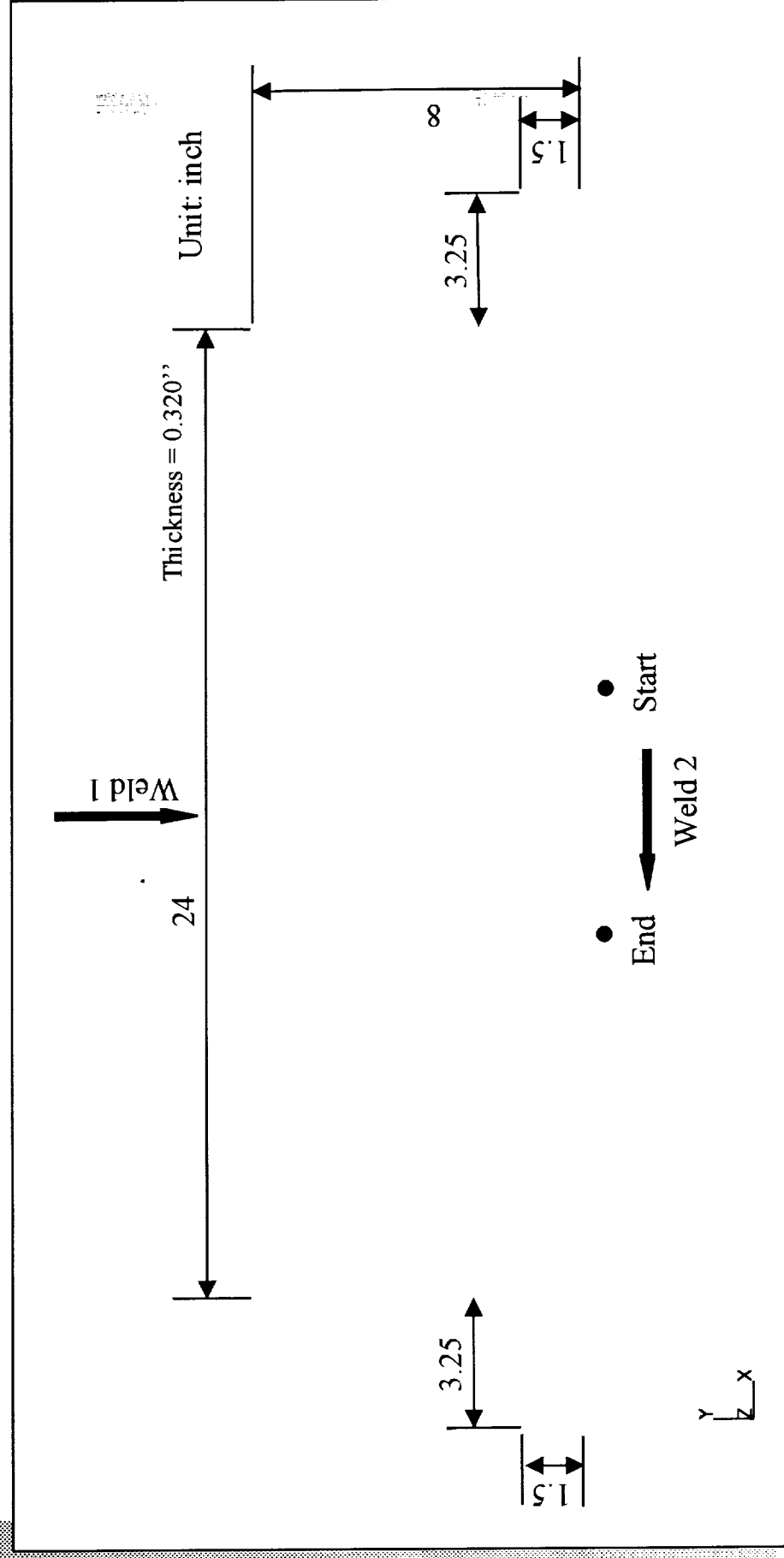
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# Thermocouple Locations on a Test Panel



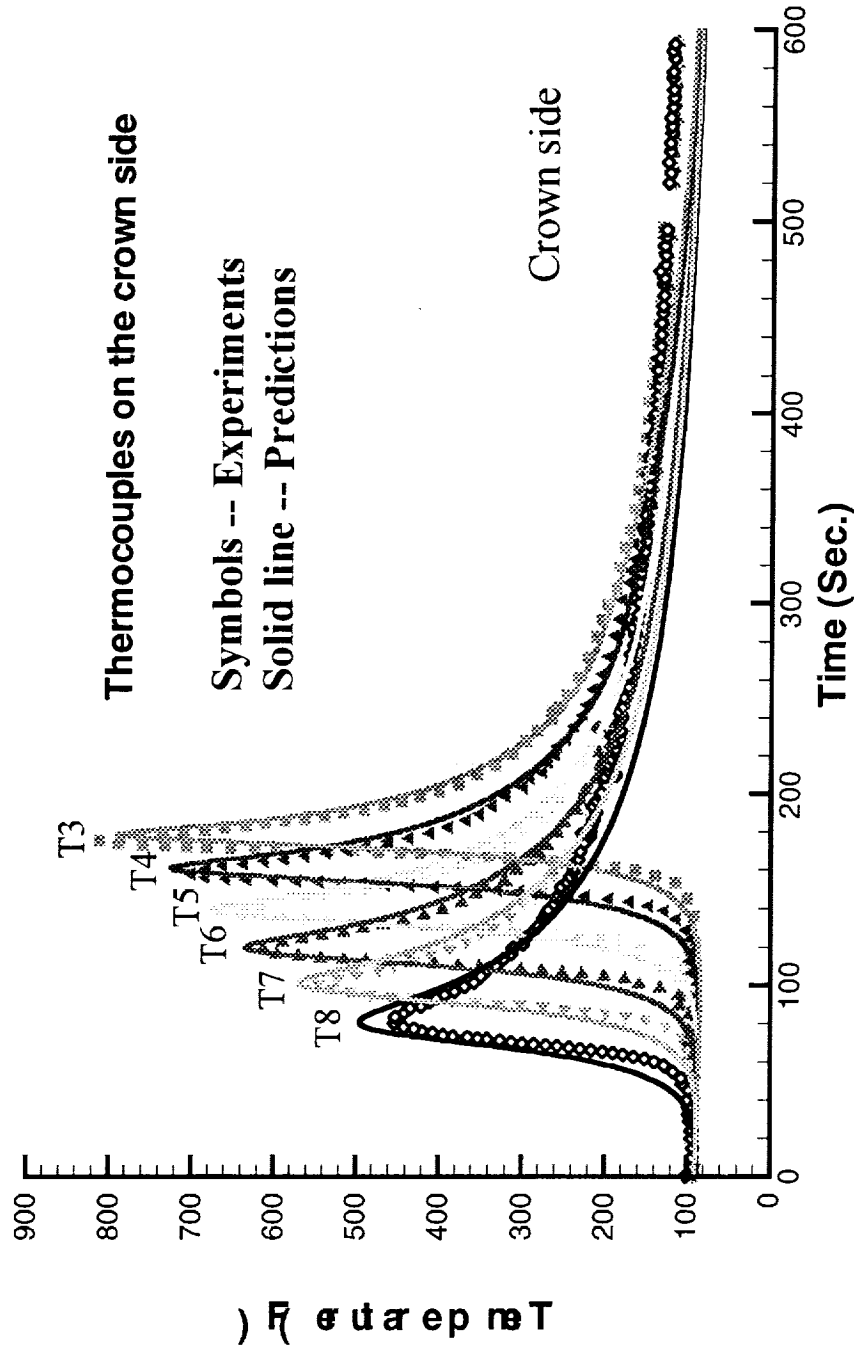
Baffle

# Finite Element Model ( 8-node element)



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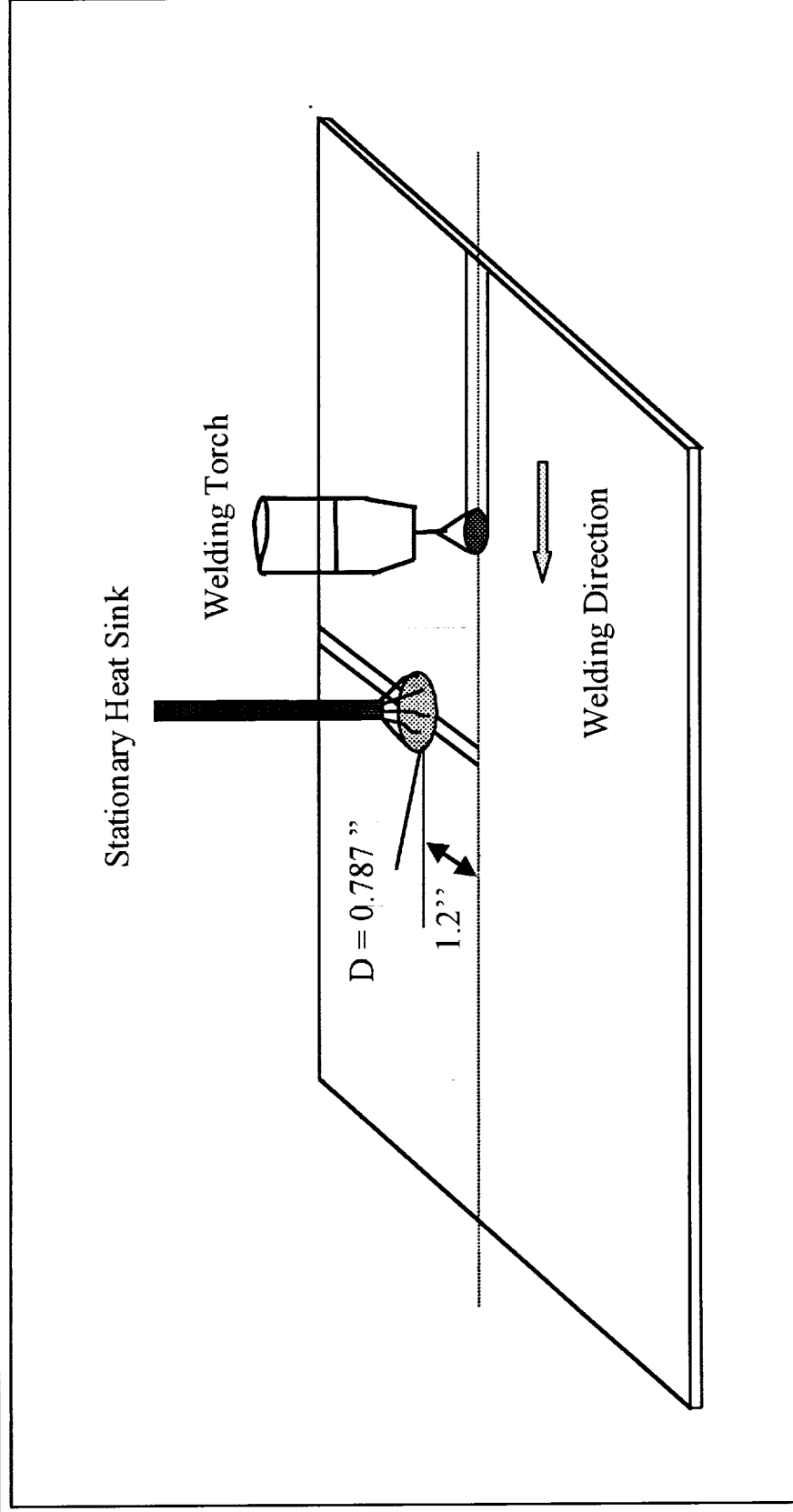
# Comparison of Temperature Histories between Experiment and Prediction



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# Proposed Stationary Cooling Technique



## *Cooling media option:*

- Liquid nitrogen
- Water
- Pressurized air knife

## *Cooling device option:*

- Heat pipe
- Heat pipe with bronze brush

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# Temperature Comparison Between Conventional Welding and Welding With Stationary Cooling

NT15 VALUE  
-INFINITY  
+2.22E-16  
+1.00E+02  
+2.00E+02  
+3.00E+02  
+4.00E+02  
+5.00E+02  
+6.00E+02  
+7.00E+02  
+8.00E+02  
+9.00E+02  
+1.00E+03  
+1.10E+03  
+1.20E+03  
+2.00E+03

(a) Conventional Welding

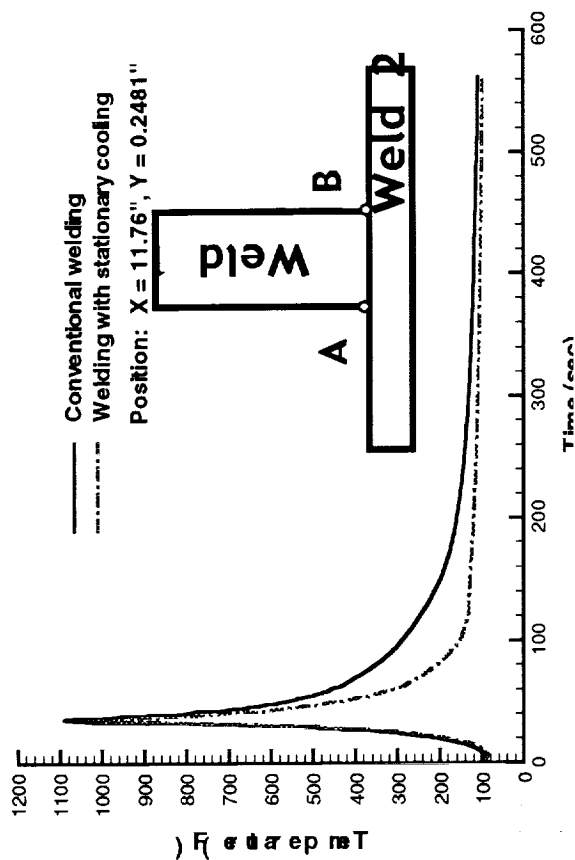
NT15 VALUE  
-INFINITY  
+2.22E-16  
+1.00E+02  
+2.00E+02  
+3.00E+02  
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+5.00E+02  
+6.00E+02  
+7.00E+02  
+8.00E+02  
+9.00E+02  
+1.00E+03  
+1.10E+03  
+1.20E+03  
+2.91E+03

(b) Welding with Stationary Cooling

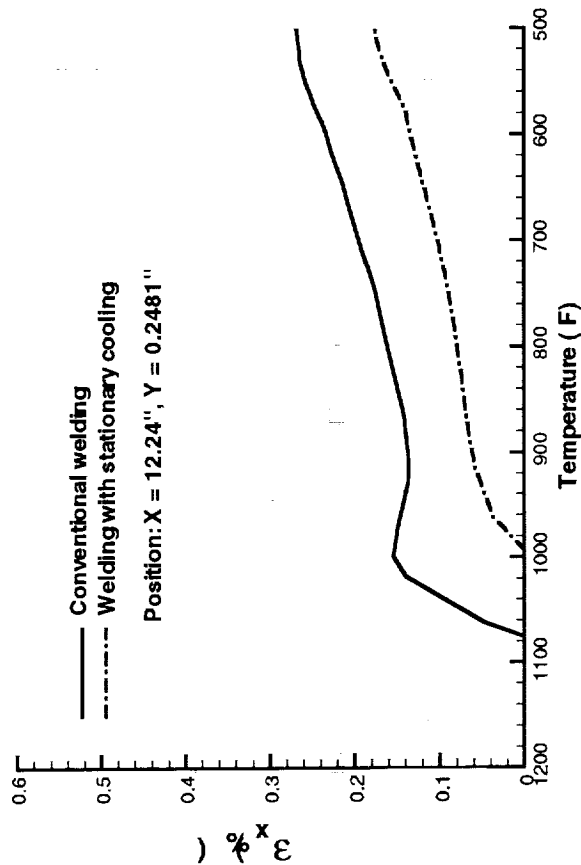
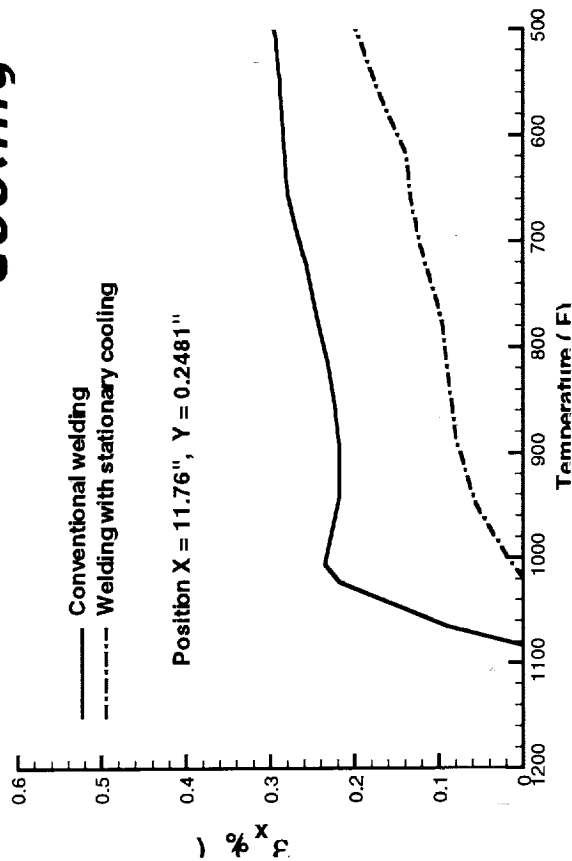
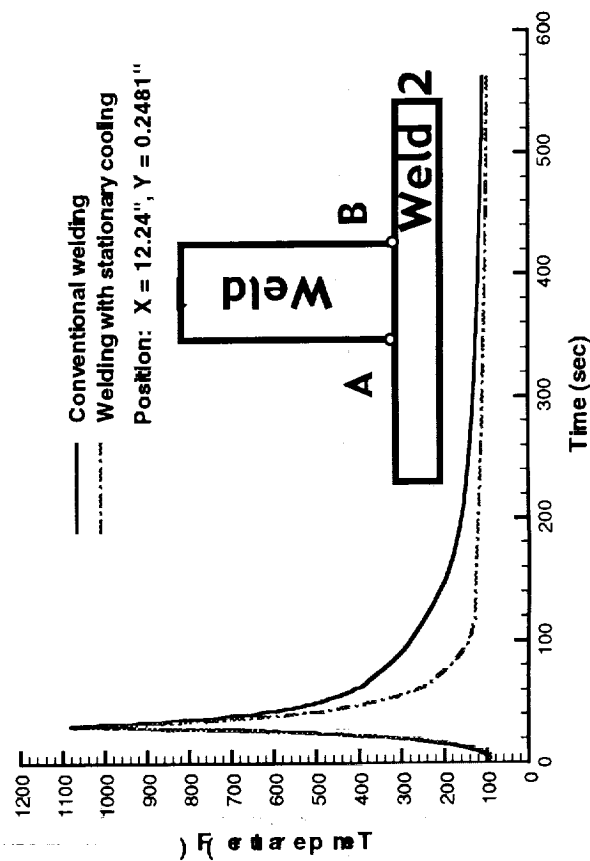
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# Temperature and Longitudinal Tensile Strain of Intersection during Welding Stationary Cooling

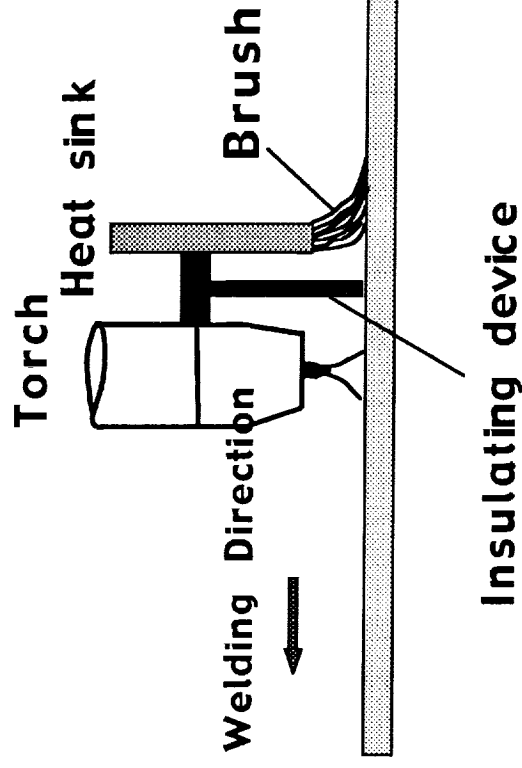
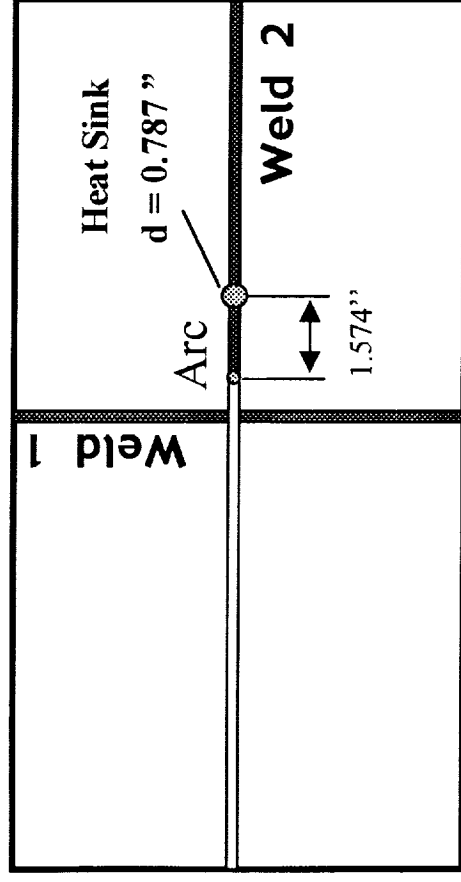
(Point A)



(Point B)



# Proposed Trailing Heat Sink Techn

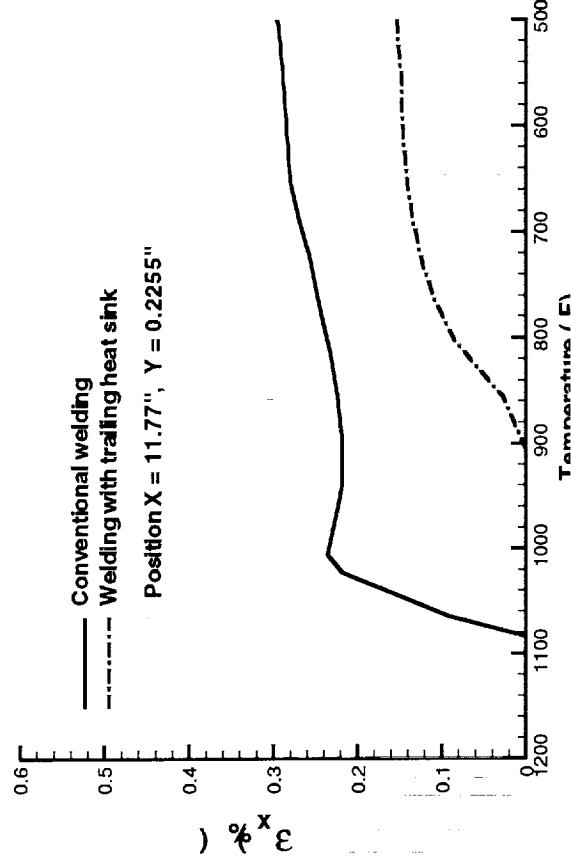
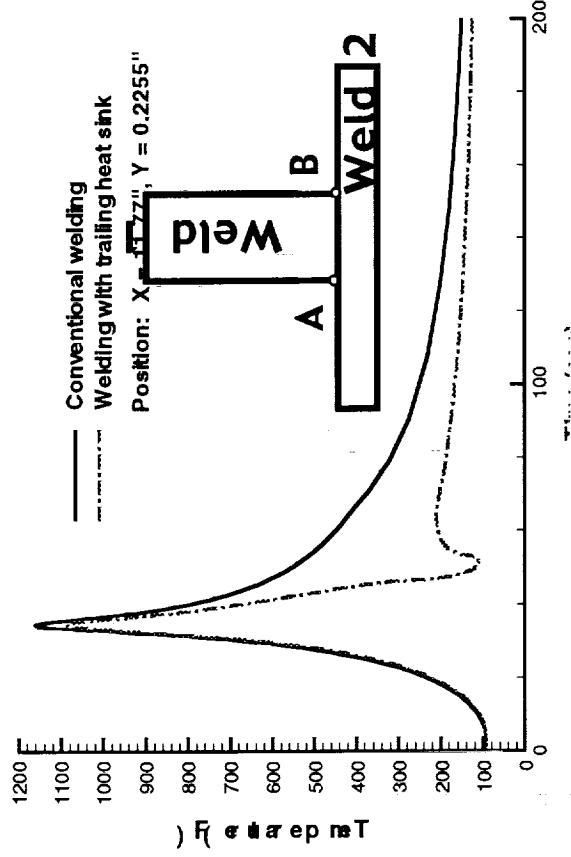


Cooling media option: Liquid nitrogen or Pressurized air knife

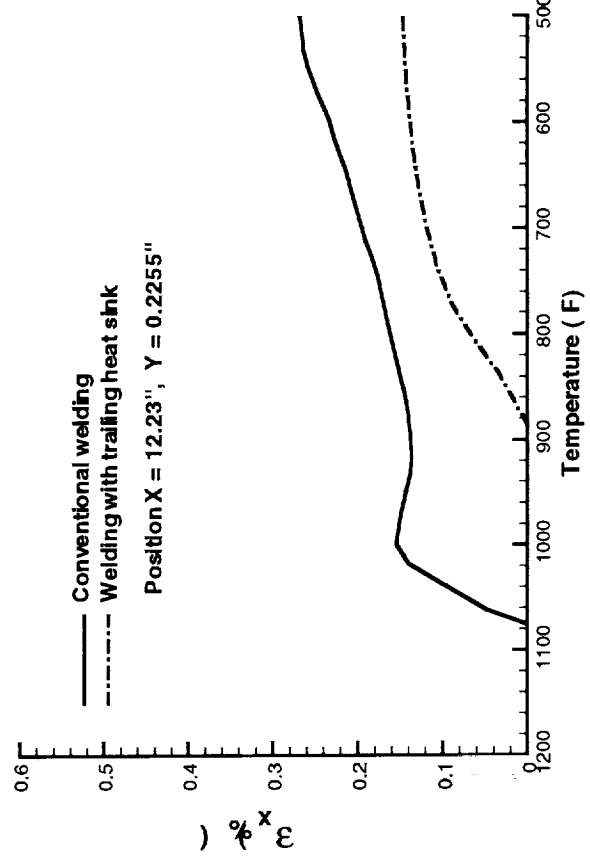
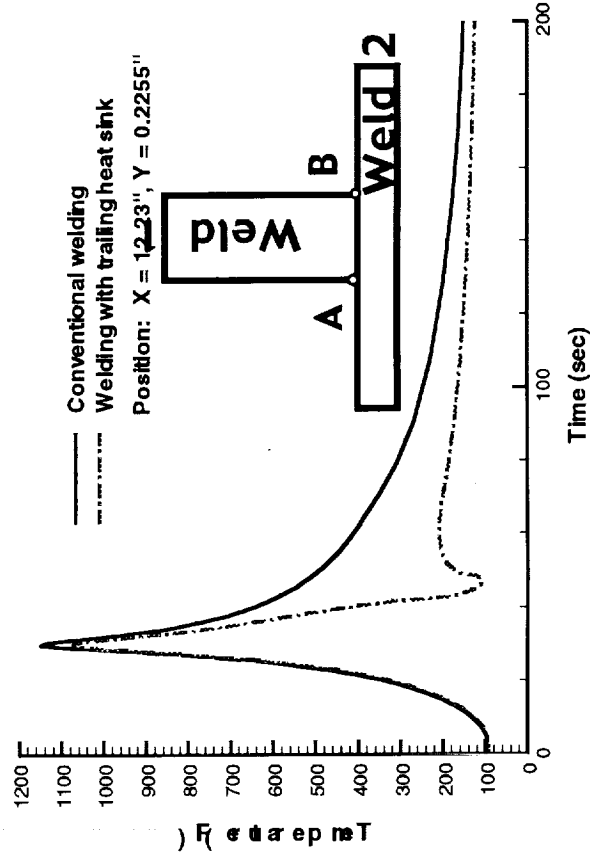
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# Temperature and Longitudinal Tensile Strain of Intersection during Welding Heat Sink Technique

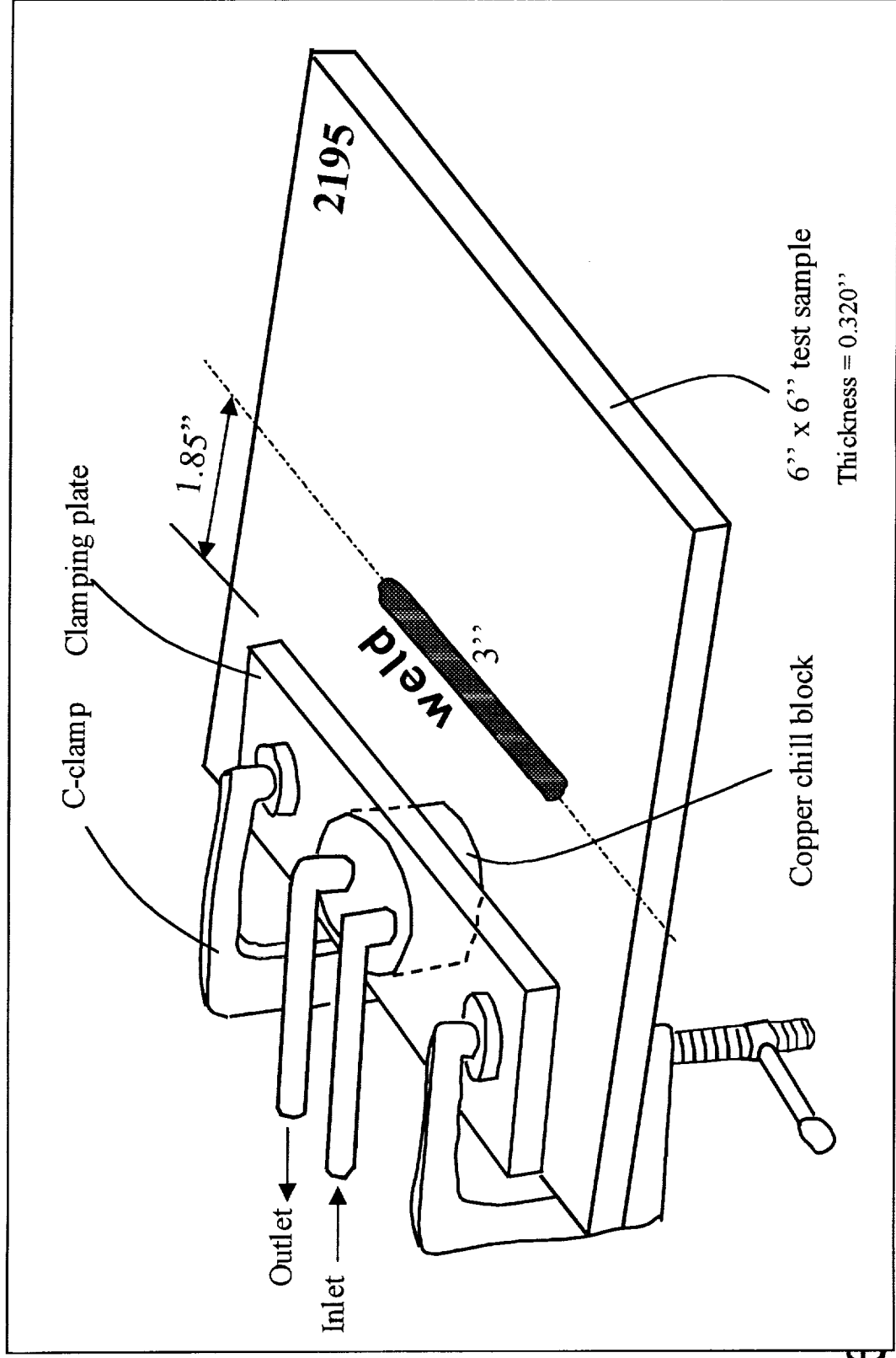
(Point A)



(Point B)

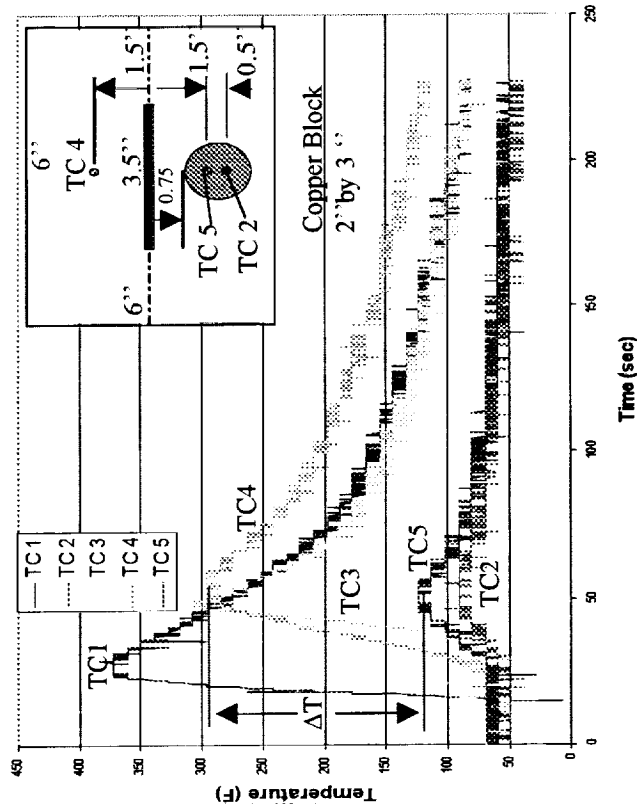


# Varestraint Machine Chill Block Test Setup

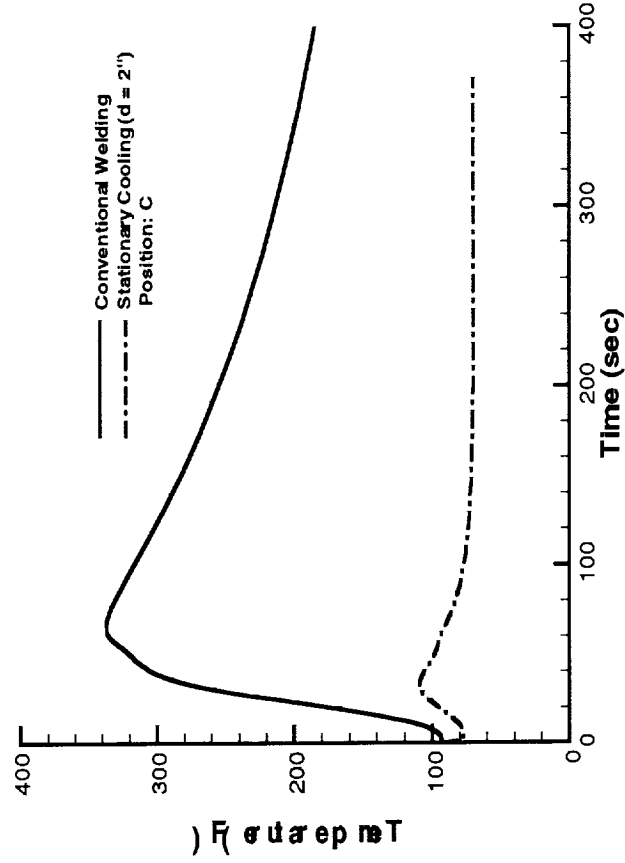


# Temperature Difference ( $\Delta T$ ) induced by Chill Block

wd12997.010 Pre - Chilled Copper Block in Fig. 28

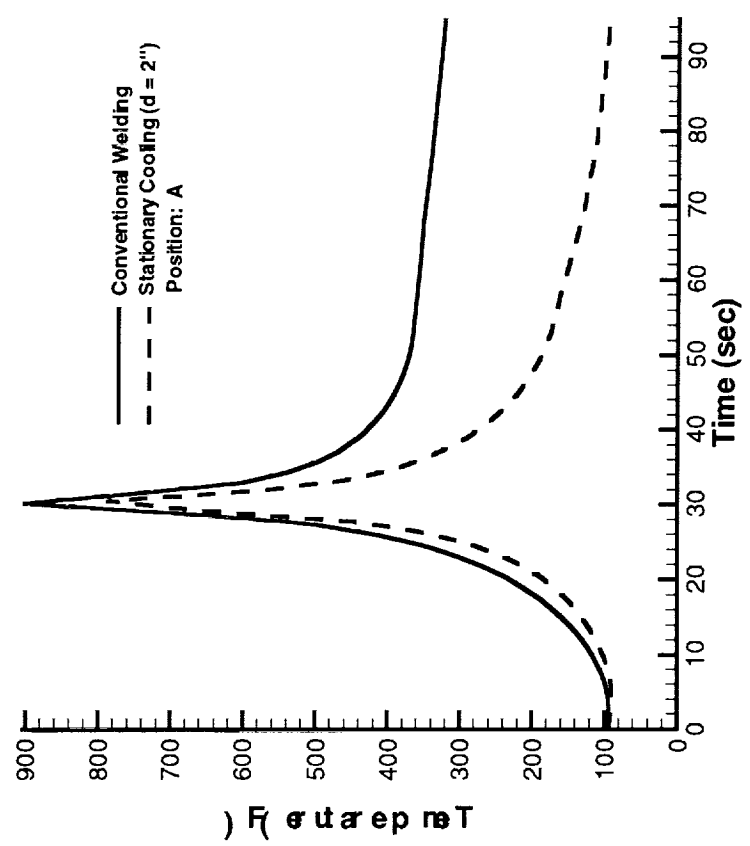


(a) Measured Temperature

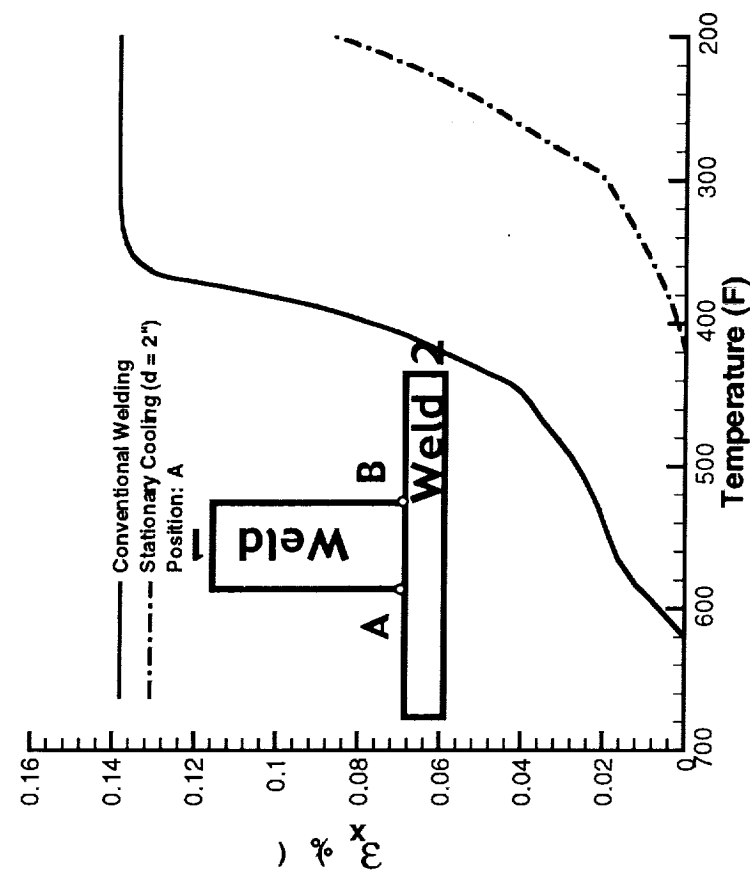


(a) Predicted Temperature

# Temperature and Strain History at Point A



(a) Temperature

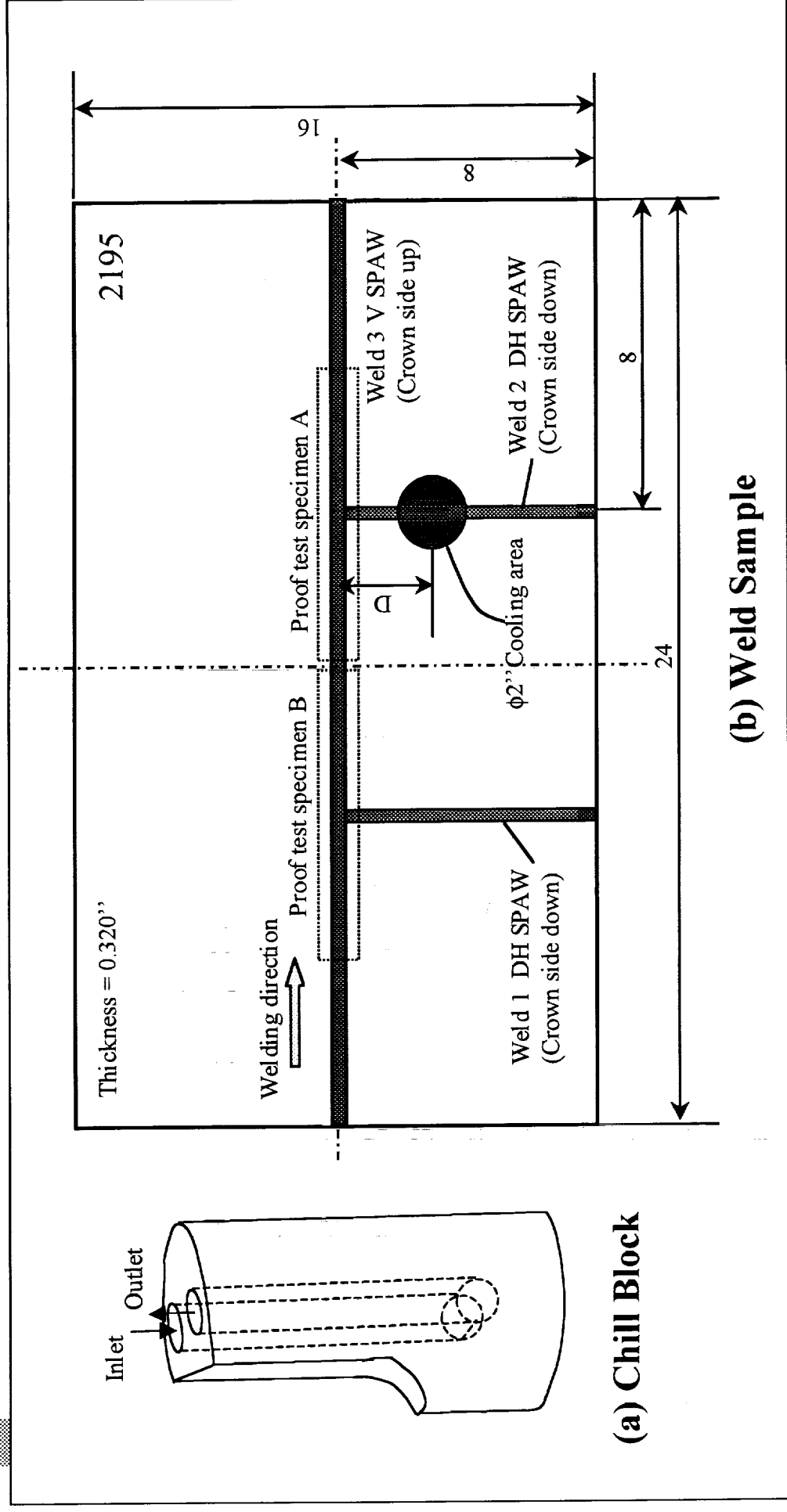


(b) Longitudinal tensile strain

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# “Quick Look” Intersection Weld Test for Stationary Heat Sinking Evaluation



**Baillie**

# Summary and Future Work

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- Two concepts, stationary cooling and trailing cooling, were proposed to prevent weld intersection cracking. Finite element analysis was used to demonstrate the potential effectiveness of those two concepts.
- Both stationary and trailing heat sink setups were proposed for preventing intersection cracking. The cooling media could be liquid nitrogen, or pressured air knife.
- Welding experiments on the small test panel with the localized heat sink confirmed the feasibility of using such a stationary cooling technique. The required cooling was achieved in this test panel.
- Systematic welding experiments should be conducted in the future to validate and refine the heat sink technique for preventing intersection cracking.

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